



Spectrum Management and Telecommunications

Radio Standards Specification

Simulation Procedure for Assessing Incident Power Density (IPD) Compliance in Accordance with RSS-102

Preface

Radio Standards Specification RSS-102.IPD.SIM, *Simulation Procedure for Assessing Incident Power Density (IPD) Compliance in Accordance with RSS-102*, issue 2, replaces RSS-102.IPD.SIM, issue 1, dated December 2023.

The main changes are listed below:

1. **new** requirements extending the frequency range to cover all portable devices operating in the 6 GHz to 300 GHz frequency band
2. **updated** the assessment requirements reference to [IEC/IEEE 63195-2](#); and
3. various editorial changes

Inquiries may be submitted by one of the following methods:

1. Online using the [General Inquiry](#) form (in the form, select the Directorate of Regulatory Standards radio button and specify “RSS-102” in the General Inquiry field)

2. By mail to the following address:

Innovation, Science and Economic Development Canada
Engineering, Planning and Standards Branch
Attention: Regulatory Standards Directorate
235 Queen St
Ottawa ON K1A 0H5
Canada

3. By email to consultationradiostandards-consultationnormesradio@ised-isde.gc.ca

Additional information and guidance are available on the Innovation, Science and Economic Development Canada (ISED) webpages [Common Questions and Answers](#) and [General Notices](#).

Comments and suggestions for improving this standard may be submitted online using the [Standard Change Request](#) form, or by mail or email to the above addresses.

All Innovation, Science and Economic Development Canada publications related to spectrum management and telecommunications are available on the [Spectrum management and telecommunications](#) website.

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47 Martin Proulx

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86 **1. Scope**

87
88 This Radio Standards Specification (RSS) sets out the computational electromagnetics
89 simulation methods for assessing compliance of portable equipment operating in the
90 frequency range from 6 GHz to 300 GHz frequency band with incident power density (IPD)
91 limits as specified in RSS-102, [Radio Frequency \(RF\) Exposure Compliance of](#)
92 [Radiocommunication Apparatus \(All Frequency Bands\)](#).

93
94 **1.1. Purpose and application**

95
96 In accordance with section 7.5 of [RSS-102](#), RSS-102.IPD.SIM outlines the requirements for
97 computational electromagnetics simulation based assessments of devices subject to
98 incident power density (IPD) compliance limits. Note that in this document, the terms
99 computational and simulation are being used interchangeably; they all refer to
100 computational electromagnetics simulations.

101
102 The annexes of RSS-102.IPD.SIM are normative. References to other documents or
103 annexes in other documents are normative as well.

104
105 RSS-102.IPD.SIM covers all portable devices operating in the 6 GHz to 300 GHz frequency
106 band. The technical requirements contained in it are used to perform accurate and
107 repeatable simulation-based assessments.

108
109 **1.2. Transition period**

110
111 This document will be in force as of the date of its publication on Innovation, Science and
112 Economic Development Canada's (ISED) website. However, a transition period of **6**
113 **months** from the publication date will be provided, within which compliance with the IPD
114 provisions in, RSS-102.IPD.SIM, issue 1, and RSS-102.IPD.SIM, issue 2, will be accepted.
115 After this period, only applications for the certification of equipment under the provisions of
116 RSS-102.IPD.SIM, issue 2, will be accepted. Furthermore, after this transition period,
117 equipment that is manufactured, imported, distributed, leased, offered for sale, or sold in
118 Canada shall comply with RSS-102.IPD.SIM, issue 2.

119
120 A copy of RSS-102.IPD.SIM, issue 1, is available upon request by emailing
121 consultationradiostandards-consultationnormesradio@ised-isde.gc.ca.

122
123 **2. Normative references**

124
125 The documents that are listed on the [Radio Frequency \(RF\) Exposure Normative](#)
126 [References and Acceptable Knowledge Database](#) web page shall be consulted as
127 applicable and available, in conjunction with this RSS.

128

129 ISED may consider assessment methods not covered by RSS-102.IPD.SIM or the
130 referenced publications. To this end, send an inquiry by emailing
131 consultationradiostandards-consultationnormesradio@ised-isde.gc.ca with detailed
132 information on the alternative assessment method(s).

133

134 **3. Definitions, abbreviations/acronyms and quantities**

135

136 Refer to [RSS-102](#) and [RSS-102.IPD.MEAS](#) for the abbreviations/acronyms and quantities
137 which are applicable to this standard.

138

139 **4. General requirements**

140

141 This section outlines the general requirements for compliance assessment of EUT
142 operating from 6 GHz to 300 GHz.

143

144 **4.1. Exposure limits, use cases and exposure conditions**

145

146 Radiocommunication apparatus shall comply with the limits outlined in Health
147 Canada's [Safety Code 6](#) and its [Safety Code 6 Notice](#) adopted in [RSS-102](#). Refer to
148 section 5 of [RSS-102](#) for the relevant limits.

149

As per Health Canada's Safety Code 6 and its Notice, for the 6 GHz to 300 GHz frequency band, two frequency-dependent limits are defined.

The first limit applies to frequencies above 6 GHz and up to 300 GHz; it is associated with an averaging area defined as a 4 cm^2 square.

The second limit, which is twice the first limit, applies to frequencies above 30 GHz; it is associated with a spatial peak (pIPD) that is not averaged over an area.

Note that for frequencies above 30 GHz, other international RF exposure guidelines allow an **averaging area of 1 cm^2** . This is **not permitted in Safety Code 6 and its Notice**.

150

151 It is important to note that compliance in the reactive near-field zone would normally be
152 made against the absorbed power density (BR) limits. However, as ISED has not yet
153 developed RSS-102.APD, compliance of portable devices operating from 6 GHz to 300
154 GHz shall be assessed against the IPD (RL) limits in 5.3.3 of RSS-102. This situation is
155 only expected for transmitters that operate below 24 GHz.

156

157 Use-cases and operating configurations shall be identified and described in the RF
158 exposure technical brief (see section 6 of this document). It shall be clear how the user
159 and/or bystander foreseeably interacts with the EUT. Key RF exposure conditions shall be

160 identified using this information. The exposure assessment shall demonstrate compliance
161 with the applicable limits for each exposure condition.

162

163 **5. Simulation-based assessments**

164

165 The simulation-based assessment shall be conducted as per [IEC/IEEE 63195-2](#).

166

167 **5.1. Computational tool and method**

168

169 The computational tool used for assessments shall be clearly identified in the RF exposure
170 technical brief. Ideally, it should employ one of the following full-wave computational
171 methods:

- 172 • finite difference time domain (FDTD)/ finite integration technique (FIT)
- 173 • finite element method (FEM)

174

175 If a different computational method from the ones identified above is being considered, an
176 [inquiry](#) form (directed to the Directorate of Regulatory Standards) shall be submitted to
177 ISED, which describes the proposed method and how it can be used to perform a
178 conservative RF exposure assessment.

179

180 **5.2. Code verification**

181

182 The selected computational tool shall meet the code verification requirements outlined in
183 Annex A of [IEC/IEEE 63195-2](#).

184

185 **5.3. Computational model**

186

187 This section provides the requirements related to the computational model.

188

189 The applicant shall submit all information relevant to the modelling (see Annexes A to C),
190 including an electronic copy of the simulation and modelling information necessary to
191 reproduce the results.

192

193 The applicant is responsible for compliance with the limits specified in [RSS-102](#), regardless
194 of the computational model used.

195

196 **Note:** The applicant, when practical, may elect to conduct the entire power density
197 assessment by measuring all the possible antenna configurations (refer to section 5 of
198 [RSS-102.IPD.MEAS](#)).

199

200

201

202 **5.3.1. EUT model**

203
204 The EUT shall be modelled in free-space and the testing configurations shall be chosen
205 according to section 5.3 of [RSS-102.IPD.MEAS](#) and modelled appropriately.

206
207 The procedure for modelling the EUT shall be described in the RF exposure technical brief.
208 Relevant mechanical dimensions and material properties shall be provided, along with the
209 associated tolerances.

210
211 Truncation of the EUT model or computational domain is allowed in order to reduce
212 computational resources. However, the reactive fields of the model should not be
213 truncated. When a truncated model is used, it shall be demonstrated and documented in
214 the radio frequency (RF) exposure technical brief that the truncation has a negligible impact
215 on the RF characteristics of the EUT model. The methodology in section 9.2.5 of [IEC/IEEE](#)
216 [63195-2](#) can be used in that regard.

217
218 **5.3.2. Evaluation surface**

219
220 The evaluation surface should be in the computational domain. Otherwise, the
221 computational domain shall be chosen to ensure the reactive field components of the EUT
222 are not affected by absorbing boundary conditions.

223
224 The averaging of the IPD on an evaluation surface shall be performed in accordance with
225 section 8.4 of [IEC/IEEE 63195-2](#).

226
227 **5.3.3. Simulation parameters and computational resources**

228
229 All relevant simulation parameters, such as those related to the meshing, boundary
230 conditions, convergence, etc., as well as the computational resources required to
231 reproduce the simulation results, shall be provided in the RF exposure technical brief.

232
233 **5.3.4. Uncertainty analysis**

234
235 This section provides the requirements related to computational uncertainty analysis.

236
237 **5.3.4.1. General requirements**

238
239 A complete uncertainty analysis shall be conducted and presented in accordance with
240 [IEC/IEEE 63195-2](#). The uncertainty budget, which shall be provided in the RF exposure
241 technical brief, shall demonstrate that the expanded uncertainty ($k = 2$) of the computational
242 model is below 30 %.

243

244 The steps taken in evaluating each component of the uncertainty budget shall be provided
245 in the RF exposure technical brief.

246

247 **5.3.4.2. Simulation uncertainty**

248

249 Deviations from the prescribed procedures for evaluating the various simulation
250 uncertainties may be necessary. For example,

251

252 a. Mesh resolution (FDTD/FIT): If the requirements provided in section 9.2.2.2 of
253 [IEC/IEEE 63195-2](#) are too computationally burdensome, this uncertainty may
254 instead be evaluated by increasing the total number of mesh cells by a factor of 2 or,
255 when applying sub-gridding, by a factor of 4 in the region of highest exposure
256 (including the source antenna(s)).

257

258 b. Boundary conditions (FDTD/FIT/FEM): If the requirements provided in section 9.2.3.
259 of [IEC/IEEE 63195-2](#) are too computationally burdensome, this uncertainty may
260 instead be evaluated by increasing the size of the bounding box by 50% in all
261 directions.

262

263 c. Convergence (FDTD/FIT): If the requirements provided in section 9.2.6 of [IEC/IEEE](#)
264 [63195-2](#) are too computationally burdensome, the following may be applied.

265

266 The simulation time required for convergence, T_{conv} , shall be long enough to ensure
267 that the maximum root-mean-square (RMS) field level remains in the same voxel
268 when the simulation time is increased to $1.5 T_{conv}$ (i.e. that the location of the
269 maximum RMS field level does not change). In addition, the field level associated
270 with this voxel shall not change by more than 2%. Either the E- or H-field may be
271 considered, whichever is dominant in the context of exposure. The percent change
272 in the maximum RMS field level when increasing from T_{conv} to $1.5 T_{conv}$ shall be
273 taken as the convergence uncertainty, with a rectangular distribution.

274

275 **5.3.4.3. EUT model uncertainty and validation**

276

277 A complete uncertainty analysis involves performing measurements to validate the EUT
278 model and determine its uncertainty.

279

280 The uncertainty component EUT model (as shown in Table 2 of [IEC/IEEE 63195-2](#)) may be
281 calculated in accordance with section 9.3 in [IEC/IEEE 63195-2](#).

282

283 In situations where the IPD value derived from E- and/or H-field, the uncertainty may be
284 evaluated according to section 9.3 in [IEC/IEEE 63195-2](#).

285

$$U_{IPD}(\%) = 100 \cdot \max(n) \left[\frac{|v_{meas}^2(n) - v_{sim}^2(n)|}{\max\{\max(n) |v_{meas}^2(n)|, \max(n) |v_{sim}^2(n)|\}} \right] \quad (1)$$

286 Where

- 287 • $v_{meas}(n)$ is the IPD value derived from E- and/or H-field from *measurements* at
 288 position n or its accurate reference solution;
- 289
- 290 • $v_{sim}(n)$ is the IPD value derived from E- and/or H-field from *simulations* at
 291 position n ;

292

293 The uncertainty of the EUT model based on direct IPD values may be evaluated as follows:

294

- 295 • The *simulated* power density values at each position n on the evaluation surface
 296 shall be normalized to the radiated power. These values are denoted as $v_{sim}(n)$.
- 297
- 298 • The *measured* power density values at each position n on the evaluation
 299 surface, obtained in accordance with section 5 of [RSS-102.IPD.MEAS](#), shall be
 300 normalized to the radiated power. These values are denoted as $v_{meas}(n)$.
- 301
- 302 • The numerical uncertainty U_{IPD} shall be used instead of U_{SAR} for near-field
 303 evaluations and is determined by the following:

304

$$U_{IPD}(\%) = 100 \cdot \max \left[\frac{|v_{meas}(n) - v_{sim}(n)|}{\max[v_{meas}(n)]} \right] \quad (2)$$

305

306 The impact of lossy conductors shall be evaluated. This shall be done by evaluating the
 307 minimum and maximum conductivity of all conductors of the EUT using their published
 308 uncertainty specifications. The deviation shall be reported in the uncertainty budget using a
 309 rectangular probability distribution.

310

311 The uncertainty associated with the field maximization technique shall be included in the
 312 total numerical uncertainty budget according to Annex C of [IEC/IEEE 63195-2](#). The
 313 computational EUT model shall be validated by measurements. The requirements for the
 314 successful validation of simulation results against the corresponding measurement data is
 315 specified below. The EUT model validation shall be calculated in accordance with section
 316 7.5.3 in [IEC/IEEE 63195-2](#). Specifically:

317 If the EUT model validation is based on IPD values derived from the E- and H-fields, this
 318 may be evaluated as follows:

319

- 320 • At each position n at which $v_{meas}(n)$ or $v_{sim}(n)$ is larger than 5% of the
321 maximum *measured* or *simulated* value $\max[v_{sim}(n), v_{meas}(n)]$, validate
322 whether the deviation between the measured value at position n , $v_{meas}(n)$ and
323 the simulated value $v_{sim}(n)$ are within the combined uncertainty of U_{meas} and
324 U_{sim} by evaluating:

$$\xi_n = \sqrt{\frac{[v_{sim}(n) - v_{meas}(n)]^2}{[v_{sim}(n) \cdot U_{sim(k=2)}]^2 + [v_{meas}(n) \cdot U_{meas(k=2)}]^2}} \leq 1 \quad (3)$$

325 Where

- 326 • $v_{meas}(n)$ is the experimentally determined IPD at position n or its accurate
327 reference solution;
328 • $v_{sim}(n)$ is the computationally determined IPD at position n ;
329 • $U_{sim(k=2)}$ is the expanded ($k = 2$) uncertainty of the simulated value; and
330 • $U_{meas(k=2)}$ is the expanded ($k = 2$) uncertainty of the measured value
331

332 If the EUT model validation is instead based on direct IPD values, the calculation becomes:
333

$$\xi_n = \frac{(IPD_{meas} - IPD_{sim})}{\sqrt{(U_{meas} \cdot IPD_{meas})^2 + (U_{sim} \cdot IPD_{sim})^2}} \leq 1 \quad (4)$$

334 where:

- 335 • ξ_n is the normalized deviation
336 • IPD_{meas} is a single measured IPD value
337 • IPD_{sim} is a single simulated IPD value
338 • U_{meas} is the expanded ($k = 2$) uncertainty of the measured value
339 • U_{sim} is the expanded ($k = 2$) uncertainty of the simulated value
340

341 Note that IPD_{meas} and IPD_{sim} shall be at the same location and configuration.
342

343 When $\xi > 1$, using formula (3) or (4), the EUT model is not within the combined standard
344 uncertainty. The EUT model shall be revised and reassessed until $\xi \leq 1$.
345

346 A detailed description of the EUT model validation procedure shall be provided in the RF
347 exposure technical brief, along with model validation results and plots or tables
348 demonstrating agreement between measured and simulated results.
349

350 **5.4. Exposure assessments**

351
352 Once the computational model has been validated, exposure assessments can be
353 performed. This section provides the requirements in this regard.
354

355 **5.4.1. Exposure scenarios and separation distances**
356

357 Assessments shall be performed for each exposure scenario and separation distance
358 identified in sections 4.1 and 4.2 of [RSS-102.IPD.MEAS](#), respectively, unless sufficient
359 rationale is provided for a reduced set of worst-case exposure scenarios and separation
360 distances in the RF exposure technical brief.
361

362 Assessment using all the relevant IPD exposure metrics (i.e. $sIPD_{n+}$, $sIPD_{mod+}$, $sIPD_{tot+}$, and
363 $psIPD$) shall be reported, including the $pIPD$ for EUT with elements operating above 30
364 GHz.
365

366 **5.4.2. Devices with multiple antennas or multiple transmitters**
367

368 For devices with elements that do not operate simultaneously, assessments shall be
369 performed for each active antenna element as specified in section 8.2.2 of [IEC/IEEE](#)
370 [63195-2](#). Note that the $pIPD$ shall also be evaluated and reported following section 8.2.2 of
371 [IEC/IEEE 63195-2](#) for EUT operating above 30 GHz.
372

373 Additional assessments shall be performed for devices with multiple uncorrelated antennas
374 or multiple transmitters or sources that operate independently and can operate in different
375 frequency ranges. Their exposure shall be combined and reported in terms of the total
376 exposure ratio, as mentioned in section 8 of RSS-102.
377

378 **5.4.3. Devices with arrays or sub-arrays**
379

380 For devices with arrays or sub-arrays, assessments shall be performed for each active
381 array or sub-array following section 8.2.3 of [IEC/IEEE 63195-2](#). For all EUT, the $sIPD_{n+}$,
382 $sIPD_{mod+}$, $sIPD_{tot+}$, and for EUT operating above 30 GHz $pIPD$, shall be computed
383 separately and reported in the RF exposure technical brief for each RF channel and for
384 each antenna. The $psIPD$ shall then be computed by applying maximization techniques
385 specified in Annex C of [IEC/IEEE 63195-2](#). A description, including the rationale and
386 uncertainty associated with the chosen maximization technique, shall be documented in the
387 RF exposure technical brief.
388

389 **6. RF exposure technical brief**
390

391 The RF exposure technical brief shall include all information required to reproduce the
392 simulation and associated measurement results, including information related to the test
393 configurations, methods and instrumentation. A comprehensive list of the required
394 information is provided in [Annex A](#) of this document.
395

396 Refer to annex A of [RSS-102](#) for additional information.

397 **Annex A Information to report for incident power density assessment**
 398

399 This annex contains a comprehensive list of the information that must be included in the
 400 radio frequency (RF) exposure technical brief to demonstrate compliance with incident
 401 power density (IPD) limits for portable devices operating in the 6 to 300 GHz frequency
 402 band.
 403

404 Section A.1 lists information on the test device and exposure category. Section A.2 lists
 405 specific information for incident power density (IPD) simulations.
 406

407 **A.1 Information on the test device and exposure category**
 408

(1) General information
<ul style="list-style-type: none"> • ISED certification ID
<ul style="list-style-type: none"> • Information related to certification (i.e. HVIN, PMN, HMN, etc.)
<ul style="list-style-type: none"> • Model number
<ul style="list-style-type: none"> • RF Exposure environment (general public/controlled use)
(2) Description of the equipment under test (EUT)
<ul style="list-style-type: none"> • Nature and intended purpose of the EUT
<ul style="list-style-type: none"> • Theory of operation of the EUT
(3) Device operating configurations and test conditions
<ul style="list-style-type: none"> • Brief description of the test device operating configurations, including: <ul style="list-style-type: none"> ○ illustration(s) of the antenna position(s) relative to the equipment under test, including dimensions and separation distances (for multiple transmitters/antennas), as applicable ○ operating mode(s) and operating frequency range(s) ○ maximum output power of the device for each operating mode and frequency range ○ maximum tune-up tolerances (i.e. variation in output power of the applicable test channels) ○ antenna type with gain and operating positions ○ applicable head, body-worn, body-supported and/or limb-worn configurations ○ battery options that could affect the IPD results ○ description of the test mode software including the version number and what the software was used to control or configure as applicable (including, but not limited to, antenna selection, signaling, power tables, dynamic antenna tuning, control time-averaged IPD algorithm parameters, etc.)
<ul style="list-style-type: none"> • Procedures used to establish the test signals
<ul style="list-style-type: none"> • Detailed description of the communication protocols used during the evaluation
<ul style="list-style-type: none"> • Maximum output power or local IPD measured before and after each IPD test

<ul style="list-style-type: none"> • Description of the scaling factor used, as applicable
<ul style="list-style-type: none"> • Description of the waveforms generated by each transmitter within the EUT, including the fundamental wave shape (sinusoidal, triangular, rectangular or otherwise) and frequency, applied modulation and 99% occupied bandwidth (OBW), duty factor, etc.
<ul style="list-style-type: none"> • Description of the conducted power of excitation level applied to each antenna based on applicable use-cases and operating states

409
410
411
412

A.2 Information to be included in the RF exposure technical brief regarding computational assessments

(1) Computational resources
<ul style="list-style-type: none"> • Computational tool and method (i.e. FDTD/FIT and FEM)
<ul style="list-style-type: none"> • Code verification results (may be included in a separate attachment)
<ul style="list-style-type: none"> • Summary of the computational resources used to perform the incident power density (IPD) computations for the equipment under test (EUT) model
<ul style="list-style-type: none"> • Summary of the minimum computational requirements for reproducing the assessment results
(2) Algorithm implementation and validation
<ul style="list-style-type: none"> • Summary of the software and the implementation of the electromagnetic solver applicable to the particular IPD evaluation, including absorbing boundary conditions, source excitation methods, methods for handling thin metallic wires, sheets or dielectric materials, etc.
<ul style="list-style-type: none"> • Descriptions of the procedures used to validate the basic computing algorithms and analysis of the computing accuracy based on these algorithms for the particular IPD evaluation
(3) Computational parameters
<ul style="list-style-type: none"> • Tabulated list of computational parameters such as: <ol style="list-style-type: none"> 1. Total simulation time 2. Dimensions of the computational domain 3. Meshing, including maximum mesh step size 4. Convergence and criteria/conditions for simulation completion 5. Boundary conditions 6. Equipment under test (EUT) model separation from the absorbing boundaries 7. Any other essential parameters relating to the computational set-up requirements for the IPD evaluation
<ul style="list-style-type: none"> • Description of the procedures used to handle computation efficiency and modelling accuracy for the EUT model
(4) Transmitter model implementation and validation
<ul style="list-style-type: none"> • Description of the essential features that must be modelled correctly for the particular EUT model to be valid

<ul style="list-style-type: none">• Descriptions and illustrations showing the correspondence between the modelled EUT and the actual device with respect to shape, size, dimensions and near-field radiating characteristics
<ul style="list-style-type: none">• Description of truncated model, if applicable, and rationale and demonstration that the truncation has a negligible impact on the RF characteristics of the EUT model
<ul style="list-style-type: none">• Verification of the EUT model to ensure its equivalency with the actual device in predicting the IPD distributions
<ul style="list-style-type: none">• Verification of the IPD distribution at the high, middle and low channels, similar to those considered in IPD measurements for determining the highest IPD
(5) Dielectric parameters
<ul style="list-style-type: none">• Tabulated list of the dielectric parameters, including a description, for both the EUT and the computational domain
<ul style="list-style-type: none">• Verification of the dielectric parameters used in the IPD computation to ensure they are appropriate for determining the highest exposure expected for normal device operation
(6) Steady-state termination procedures
<ul style="list-style-type: none">• Description of the criteria and procedures used to determine that sinusoidal steady-state conditions have been reached throughout the computational domain to terminate the computations
<ul style="list-style-type: none">• Report of the number of time steps or sinusoidal cycles executed to reach a steady state
<ul style="list-style-type: none">• Description of the expected error margin provided by the termination procedures
(7) Evaluation surface and test device positioning
<ul style="list-style-type: none">• Rationale and description of the EUT test positions used in the IPD computations
<ul style="list-style-type: none">• Illustrations showing the evaluation surface and separation distances between the EUT model and the measurement system for the tested configurations
<ul style="list-style-type: none">• Detailed description of the exposure assessment procedure and results, including all exposure conditions and separation distances, with rationale for reduction to the worst-case configurations
(8) Computing spatial peak incident power density from field components
<ul style="list-style-type: none">• Description of the procedures used to compute the sinusoidal steady-state peak E-fields, H-fields, and pIPD on the evaluation surface
<ul style="list-style-type: none">• Description of the procedures used to search for the highest spatial peak incident power density (pIPD)
<ul style="list-style-type: none">• Description of the expected error margin provided by the algorithms used to compute the IPD at each location according to the selected field components and dielectric parameters
<ul style="list-style-type: none">• Description of the expected error margin provided by the algorithms used in computing the pIPD
(9) Peak spatial-average incident power density procedures
<ul style="list-style-type: none">• Description of the procedures used to search for the highest peak spatial-average incident power density (psIPD), including the procedures for handling inhomogeneous tissues within four squared centimetres (4 cm²)

<ul style="list-style-type: none"> Description of the expected error margin provided by the algorithms used in computing the psIPD
(10) Total computational uncertainty
<ul style="list-style-type: none"> Complete uncertainty budget in accordance with 63195-2
<ul style="list-style-type: none"> Description of how each uncertainty value was obtained, including any deviations from the above standard
<ul style="list-style-type: none"> Detailed description and illustration of the EUT model validation procedure and results
<ul style="list-style-type: none"> Statement of the expanded uncertainty, which shall be $\leq 30\%$
(11) Computational results
<ul style="list-style-type: none"> Description of how the maximum device output rating is determined and used to normalize the IPD values for each test configuration
<ul style="list-style-type: none"> Plots of the IPD on the evaluation surface, both before and after spatial averaging is applied, for each test configuration to be measured
<ul style="list-style-type: none"> Tabulated list of the pIPD and psIPD values, along with their locations on the evaluation surface(s)
<ul style="list-style-type: none"> Tabulated list of the root mean square (RMS) E-field and H-field levels at each pIPD location
<ul style="list-style-type: none"> Description of applied method to evaluate psIPD (e.g. field maximization technique, optimization, codebook, etc.)
<ul style="list-style-type: none"> Description of applied averaging algorithm according to section 8.6 of IEC/IEEE 63195-2
(12) Antenna information
<ul style="list-style-type: none"> Antenna efficiency at the corresponding frequency
<ul style="list-style-type: none"> Far-field gain (in dB) at the corresponding frequency
<ul style="list-style-type: none"> Far-field pattern (as per Annex B) on the solid angle evaluated with step sizes of five degrees along phi (ϕ) and theta (θ)
(13) Feedpoint impedance or input reflection coefficient
<ul style="list-style-type: none"> Complex feedpoint impedance or the reflection coefficient at the corresponding frequency, as per Annex B (with a span of ± 5 GHz and a maximum step size of 50 MHz)

413
 414
 415

416 **Annex B Specific information related to power density computations**

417

418 This annex contains specific information related to power density computations.

419

420 **B.1 Far-field patterns**

421

422 The complex E-field of the far-field pattern shall be provided in a comma- or space-
423 separated format, with one entry per line:

424
$$i, j, \phi, \theta, E_{\phi r}, E_{\phi i}, E_{\theta r}, E_{\theta i}$$

425 where:

426 • i and j are rectilinear grid point indices corresponding to the ϕ and θ coordinates on
427 the solid angle

428 • ϕ and θ are the coordinates on the solid angle in radians

429 • $E_{\phi r}$ and $E_{\phi i}$ are the real and imaginary parts of the ϕ component of the E-field

430 • $E_{\theta r}$ and $E_{\theta i}$ are the real and imaginary parts of the θ component of the E-field

431

432 **B.2 Feedpoint impedance**

433

434 The feedpoint impedance shall be provided in a comma- or space-separated format, with
435 one entry per line:

436
$$f, Z_r, Z_i$$

437 where:

438 • f is the frequency in GHz

439 • Z_r and Z_i are the real and imaginary parts of the feedpoint impedance in Ω

440

441 **B.3 Reflection coefficient**

442

443 The reflection coefficient shall be provided in a comma- or space-separated format, with
444 one entry per line:

445
$$f, |S_{11}|$$

446 where:

447 • f is the frequency in GHz

448 • $|S_{11}|$ is the absolute value of the input reflection coefficient in dB

449

450

451 **Annex C Computer-aided design model requirements**
452

453 The equipment under test (EUT) model used for the computations should be equivalent,
454 and ideally identical, to the actual device that would be assessed with the measurement
455 system. The computer-aided design (CAD) file shall be made available upon ISED's
456 request in an exchangeable format such as *.sat, *.sab, *.step, *.stl (for other file formats,
457 please verify with ISED to ensure they are supported). Note that the provisions for
458 disclosure of information as described in Radio Standards Procedure RSP-100,
459 [Certification of Radio Apparatus and Broadcasting Equipment](#), apply.
460

461 Objects and layers in the CAD file shall be organized in a table where the materials and
462 dielectric properties (including any frequency dependencies) are identified. Whenever
463 possible, all conducting parts should be integrated into the CAD model with their associated
464 frequency-dependent dielectric properties.

